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TECHNICAL REPORT ARCCB-TR-95007

FRACTURE TOUGHNESS ASSESSMENT OF PRESENT AND FUTURE PRESSURE VESSEL MATERIALS BASED ON CHARPY IMPACT ENERGY AND YIELD STRENGTH

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alloy steel, have been heat treated to Charpy impact energy. The correla Underwood suggests that for A722 limitation of their study was that temperature. This study evaluates utilizing these correlations. Results at room temperature, and tends to one instance, was a conservative estimated.	o various strength and toughness lettions investigated included those by steel, the Rolfe-Novak correlation the Charpy impact energy was much appropriate the charpy impact energy and toughness of this study indicate that the Rollinderpredict the measured fracture imate of the measured fracture tought is recommended that if a correlation	evels and evaluated for correct Rolfe-Novak and Ault-Wassen predicts the fracture tous neasured at -40°F, whereas ess at both room temperature life-Novak correlation overp toughness at -40°F. The Astronovacy of the material at both is necessary for estimating	teel, and ASTM A723 high strength low elations between fracture toughness and ld-Bertolo. Previous work by Kapp and ghness reasonably well. One potential the toughness was evaluated at room e and at -40°F and considers both when redicts the measured fracture toughness cault-Wald-Bertolo correlation, in all but a room temperature and -40°F. Utilizing the toughness of any of these materials,
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INTRODUCTION

Because of the complexities of fracture testing, and the inability of many labs to conduct a fracture toughness test, many labs will simply measure the Charpy impact energy (CVN) and use one of many CVN- K_{lc} correlations (ref 1) to predict the toughness of the material being investigated. This study examines two well-known correlations that are applicable in the upper-shelf regime. The two correlations studied are the Rolfe-Novak correlation (ref 2)

$$\left(\frac{K_{lc}}{\sigma_{ys}}\right)^2 = 5\left(\frac{CVN}{\sigma_{ys}} - 0.05\right) \tag{1}$$

and the Ault-Wald-Bertolo correlation (ref 3)

$$(\frac{K_{lc}}{\sigma_{ys}})^2 = 1.37(\frac{CVN}{\sigma_{ys}}) - 0.045$$
 (2)

where σ_{yz} is the 0.2 percent yield strength.

These correlations were developed by compiling a large amount of data and curve-fitting the best linear fit to derive these equations. The Rolfe-Novak study included data from steels with yield strengths in excess of 100 Ksi, while the Ault-Wald-Bertolo study included only ultra-high strength steels (tensile strengths in the range of 200 Ksi to 300 Ksi). Although some of the materials utilized in this study do not fit these classifications, the correlation is still being investigated.

Since the materials being considered all possessed relatively high fracture toughness, even at -40°F, full J-integral ($J_{\rm Ic}$) fracture toughness tests were conducted according to ASTM E-813, "Standard Test Method for $J_{\rm Ic}$, A Measure of Fracture Toughness."

Elastic fracture mechanics (K_{Ic}) does not adequately predict the toughness of these materials because we cannot meet the K_{Ic} test requirements, per ASTM E-399, "Standard Test Method for Plane-Strain Fracture Toughness of Metallic Materials." Therefore, we have utilized elastic-plastic fracture mechanics (J_{Ic}) and converted the results to K_{I} with the following equation:

$$K_J = \sqrt{\frac{EJ_{lc}}{1 - v^2}} \tag{3}$$

These K_1 values are believed to be good estimates of K_{le} .

RESULTS

The results of testing can be observed in Table 1. Note that both CVN and K_J were evaluated at both room temperature (72°F) and -40°F. The data presented in this table are the result of averaging a minimum of three test results for each condition.

The results presented in Table 1 are also shown graphically in Figures 1 and 2. The Rolfe-Novak correlation conservatively predicts the measured fracture toughness of all materials investigated, except for the AF1410. In the case of AF1410, it appears that the Ault-Wald-Bertolo correlation predicts the measured fracture response very accurately.

Figure 3 is significant since it attempts to predict the room temperature fracture toughness response based on -40°F CVN. Again, the Rolfe-Novak correlation does seem to conservatively predict the fracture toughness response (with a few outlier, especially at higher toughness values). As seen in Figure 3, the PH 13-8 Mo stainless steel is not conservatively predicted at room temperature based on a -40°F CVN.

CONCLUSIONS

- 1. Previous work by Kapp and Underwood (ref 4) indicated that for A723 steel, the Rolfe-Novak correlation predicts the fracture toughness response at room temperature reasonably well based on a -40°F CVN. This study verifies those findings. We have also found that Rolfe-Novak conservatively predicts the room temperature fracture toughness of Inconel 718 and the higher strength levels of AF1410 when based on -40°F CVN. However, the PH 13-8 Mo and the lower strength levels of AF1410 do obey this trend.
- 2. We have determined that the Rolfe-Novak correlation does not adequately or conservatively predict the fracture toughness at room temperature when estimated by room temperature CVN. Under these conditions, the Ault-Wald-Bertolo correlation does indeed conservatively predict the fracture toughness for all materials investigated.
- 3. Rolfe-Novak does conservatively predict the -40°F fracture toughness of A723, Inconel 718, and PH 13-8 Mo when based on -40°F CVN. Whereas it does not adequately predict the -40°F fracture toughness of AF1410 when based on -40°F CVN. For this material, the Ault-Wald-Bertolo correlation does predict accurate fracture toughness.
- Based on the findings of this study, it appears that the accuracy of the two correlations studied is dependent on material tested, heat treatment condition, and test temperature. One general conclusion that can be drawn from this analysis is that the Ault-Wald-Bertolo correlation in most every case studied, conservatively estimated the fracture toughness of each of these materials, heat treatments, and test temperatures. However, the prediction is extremely conservative in many cases. This suggests that whenever an accurate representation of these classes of materials is necessary, a $J_{\rm Ic}$ fracture toughness test must be performed.

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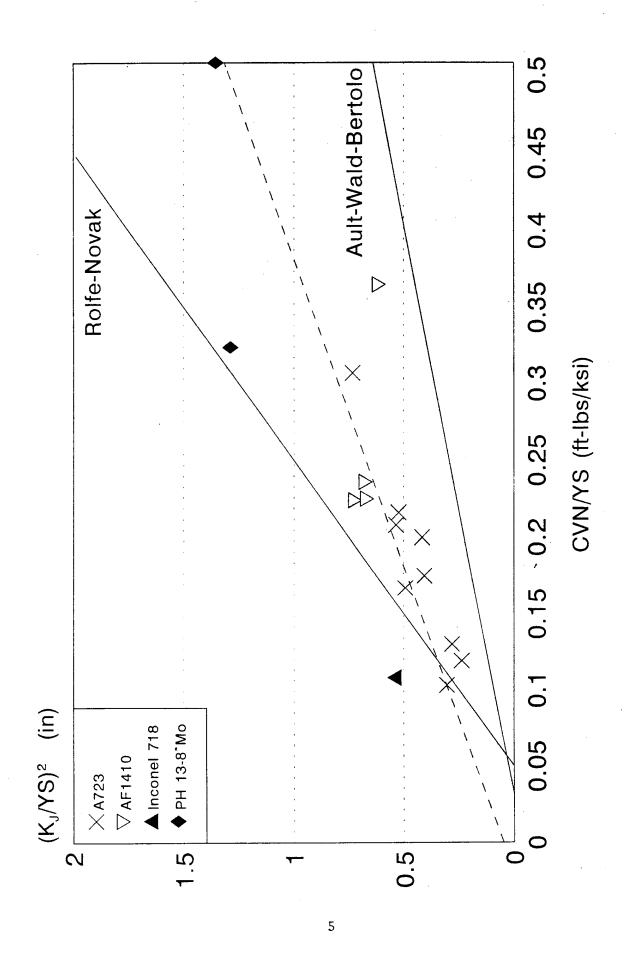
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Table 1 - Compilation of strength and toughness data used for analysis

2 (Ky (-40F)/YS) (in)	0.303	0.173		0.252	0.542	1.823	1.641	0.452	0.121	0.376	0.506	0.190	0.391	0.593	0.328	0.936
(Ky (72F)/YS)	0.613	0.721	0.674	0.667	0.542	1.355	1.289	0.493	0.281	0.416	0.535	0.237	0.406	0.523	0.304	0.733
CVN(-40F)/YS (ft-lbs/ks1)	0.275	0.142	0.156	0.188	0.108	0.384	0.324	0.131	0.070	0.084	0.141	0.051	0.069	0.149	0.103	0.242
CVN(72F)/YS (ft-lbs/ksi)	0.365	0.224	0.236	0.225	0.108	0.508	0.324	0.167	0.130	0.200	0.208	0.119	0.175	0.216	0.103	0.307
Ky (-40F) (1bs/in)	104	91		107	123	239	237	113	40	95	106	51	100	114	106	148
Ky (72F) (ibs/in)	148	186	174	174	123	206	210	118	61	100	109	57	102	107	102	131
CVN (-40F) (ff-lbs)	52	31	33	40	18	68	9	22	80	13	21	9	-	22	19	37
CVN (72F) (ft-lbs)	69	49	20	48	18	06	09	28	15	31	31	14	. 82	33	19	47
.2% Y.S. (ksi)	189	219	212	213	191	117	185	168	115	155	149	117	160	148	185	153
Condition	HT#1	HT#2	HT#3	HT#4		HT#5	HT#6									
Material	AF1410				Inconel 718	PH 13-8 Mo		A723			4	•				

HT#1	HT#2	HT#3	HT#4	HT#5	. 9#1H
1650F-1hr,AC	1650F-1hr,AC	1650F-1hr, AC 1650F-1hr, AC 1650F-1hr, AC 1700F-1hr, AC 1700F-1hr, AC	1650F-1hr,AC	1700F-1hr,AC	1700F-1hr,AC
1525F-1hr,AC	1525F-1hr,AC	1525F-1hr, AC 1525F-1hr, AC 1700F-1hr, AC	1525F-1hr,AC	1700F-1hr,AC	1700F-1hr, AC
-100F-1hr,AW	-100F-1hr,AW	-100F-1hr,AW -100F-1hr,AW -100F-1hr,AW 1025F-5hr,AC	-100F-1hr,AW	1025F-5hr, AC	1025F-3hr, AC
400F-5hr,AC	925F-5hr, AC	950F-5hr,AC	975F-5hr, AC		•



Solid lines represent correlations, dotted lines represent best linear fit of data being studied Figure 1-K, (72F) vs CVN (72F)

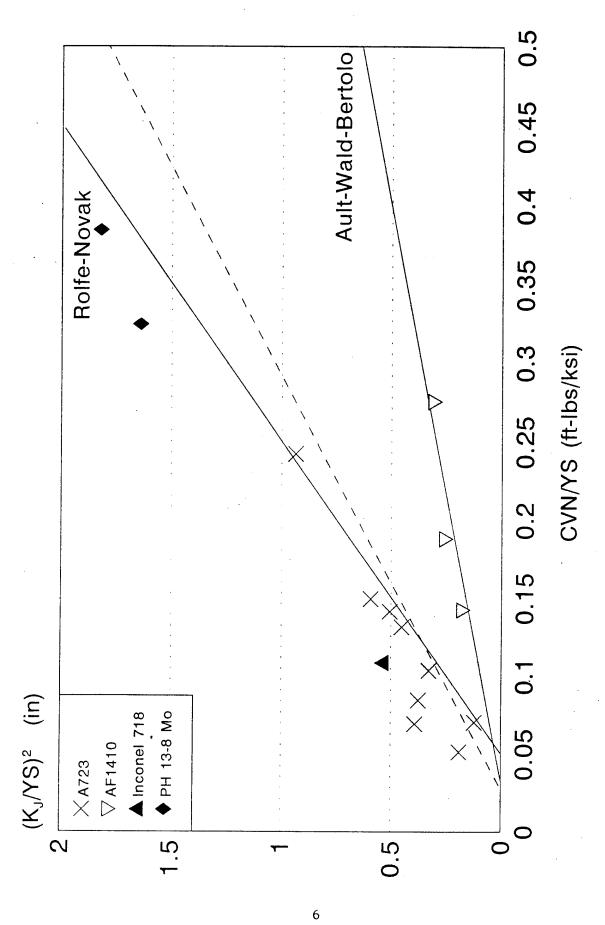
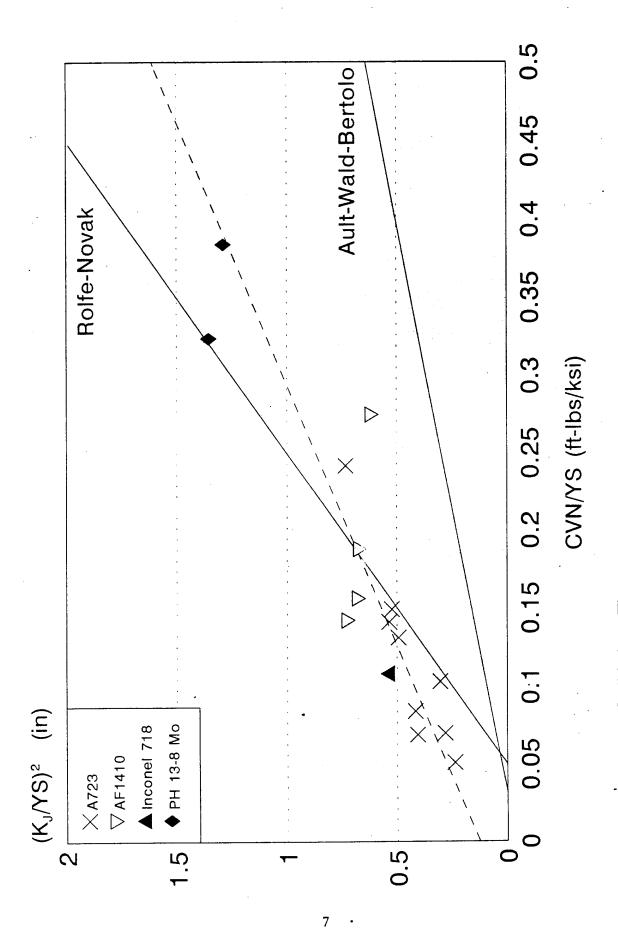


Figure 2 - K_J (-40F) vs CVN (-40F) Solid lines represent correlations, dotted lines represent best linear fit of data being studied



Solid lines represent correlations, dotted lines represent best linear fit of data being studied Figure 3 - K₃ (72F) vs CVN (-40F)

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